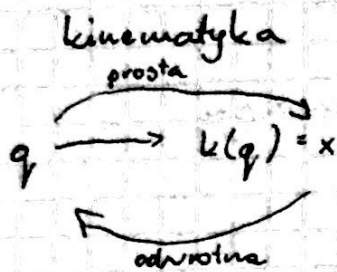


# ROBOTYKA (1)

[1]

16. 01. 2017r.



dynamika

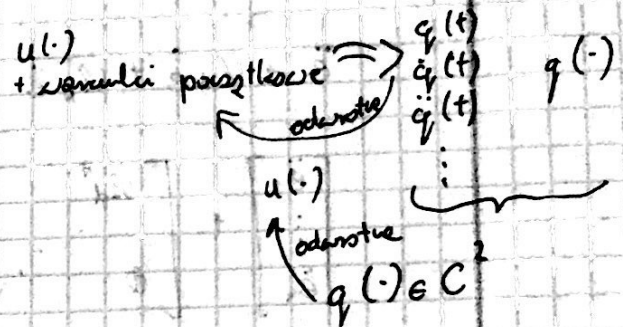
$$u = Q(q)\ddot{q} + C(q, \dot{q})\dot{q} + D(q)$$

$q(t)$  - będzie zależał od warunków początkowych

w tym przypadku:

$$q(0)$$

$$\ddot{q}(0)$$



$$Q(q)\ddot{q} + C(q, \dot{q})\dot{q} + D(q) = u$$

$$+ q_d(\cdot) \in C^2$$

desired



METODA OBLICZANIA MOMENTU (CT)

1<sup>o</sup> linearyzacja modelu - wprowadzamy nowe sterowanie ( $v$ )

$$Q(q)v + C(q, \dot{q})\dot{q} + D(q) = u$$

$$Q(q)\ddot{q} = Q(q)v \quad | Q^v$$

$$\ddot{q} = v$$

niezależna = niezależna

2° Zamknijcie pętlę sprzężenia zwrotnego

$$\text{Ogłd: } e(\cdot) = q(\cdot) - q_d(\cdot)$$

$$v = \ddot{q}_d - K_d(\dot{q} - \dot{q}_d) - K_p(q - q_d)$$

↑  
stłc <sup>asp.</sup> ~~manier~~ <sup>manier</sup> ~~o~~ <sup>o</sup>  
(dobieramy)

$$\ddot{e} + K_d \dot{e} + K_p e = 0$$

$$\begin{bmatrix} \ddot{e}_1 \\ \vdots \\ \ddot{e}_n \end{bmatrix} + \begin{bmatrix} K_d^1 & & 0 \\ & \ddots & \\ 0 & & K_d^n \end{bmatrix} \begin{bmatrix} \dot{e}_1 \\ \vdots \\ \dot{e}_n \end{bmatrix} + \begin{bmatrix} K_p^1 & & 0 \\ & \ddots & \\ 0 & & K_p^n \end{bmatrix} \begin{bmatrix} e_1 \\ \vdots \\ e_n \end{bmatrix} = \begin{bmatrix} 0 \\ \vdots \\ 0 \end{bmatrix}$$

$K_p, K_d$  - macierze diagonalne

$$\ddot{e}_i + K_d^i \dot{e}_i + K_p^i e_i = 0 \quad i = 1, \dots, n$$

$$\ddot{e} + K_d \dot{e} + K_p e = 0 \quad \rightarrow \text{równanie skalare}$$

$$e(t) \xrightarrow{t \rightarrow \infty} 0$$

Jak dobrać  $K_p, K_d$  ?

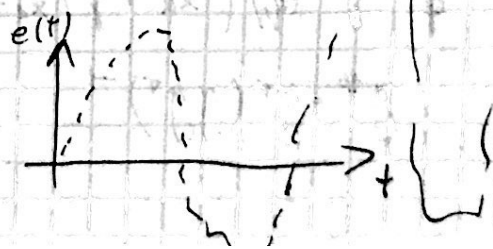
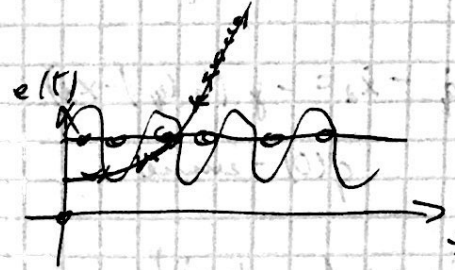
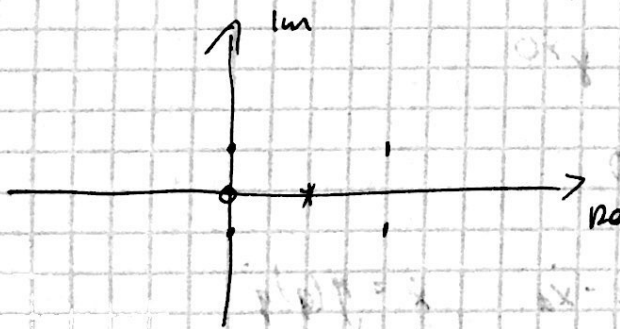
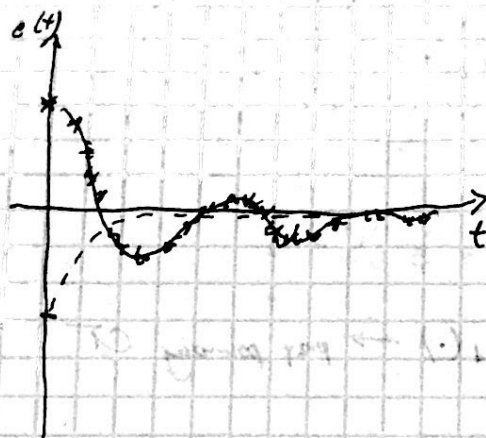
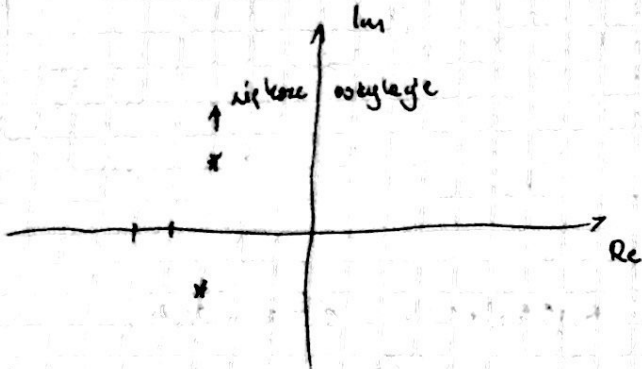
→ równanie charakterystyczne

$$s^2 + K_d s + K_p = 0$$

→ pierwiastki równania charakterystycznego

$$\Delta = k_d^2 - 4k_p k_v$$

$$s_{1,2} = \frac{-k_d \pm \sqrt{\Delta}}{2}$$



$$\Delta > 0 \quad k_p > 0$$

$$\Gamma \Delta < k_d$$

STABILNY ~~system~~  $k_p, k_d > 0$

Klasyczny sterownik PD

ZADANIE ŚLEDZENIA TRAJEKTORII EFEKTORA

$x_d(t)$

$$Q(q)\ddot{q} + (C(q, \dot{q})\dot{q} + D\dot{q}) = \tau$$

$$x = k(q)$$

→ Metoda pośrednia

$$x_d(\cdot) \rightarrow q_d(\cdot) \rightarrow \text{przy pomocy CT}$$

$$e(t) = x(t) - x_d(t)$$

$$\dot{e} = -\gamma e, \quad \gamma > 0$$

$$e(t) \xrightarrow{t \rightarrow \infty} 0$$

$$\dot{e} = \dot{x} - \dot{x}_d \quad \dot{x} = J(q)\dot{q}$$

$$J(q)\dot{q} - \dot{x}_d = -\gamma(k(q) - x_d)$$

$q(0)$  - znane

$$\dot{q} = J^*(q) (\dot{x}_d + \gamma(x_d - k(q)))$$

$$J^* = J^T (J J^T)^{-1}$$

Wyznaczenie  $q_d(\cdot)$

→ Metoda bezpośrednia

$$x = k(q)$$

$$\rightarrow \dot{x} = J(q)\dot{q}$$

$$e(t) = x(t) - x_d(t)$$

$$\ddot{x} = \dot{J}(q)\dot{q} + J(q)\ddot{q}$$

$$\ddot{q} = Q^{-1}(u - C\dot{q} - D)$$

$$\ddot{x} = \dot{J}(q)\dot{q} + J(q) \cdot Q^{-1}(u - C\dot{q} - D)$$

$$= P(q, \dot{q}) + K(q)u = v$$

↓  
u = u<sub>new</sub> sterowanie

~~nowe~~  $\ddot{x} = v$

$$v = \ddot{x}_d - k_1(\dot{x} - \dot{x}_d) - k_0(x - x_d)$$

$$\ddot{e} + k_d \dot{e} + k_p e = 0$$